INTRODUCTION TO ROBOTICS (Kinematics, Dynamics, and Design)

SESSION # 18: ROBOT TRAJECTORY GENERATION

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Hey! Where Should I go?

Motion Planning: refers to the study of generating motion for the robot to accomplish a task. This consists of:

Path Planning; generating a feasible path from an initial position to a final position by describing the geometric position and orientation of the robot during the transition.

Trajectory Generation; attaching a time frame to the paths generates a trajectory. The trajectory not only describes the position of the robot during motion, but also how that position changes with time.



We shall study Methods to:

- Compute a *Trajectory* that describes the desired motion of a manipulator in space...
- *Trajectory* is the time history of position, velocity, and acceleration for each joint (i.e. degrees-of-freedom).
- *Trajectory Planning* means the determination of the actual trajectory, or path, along which the robot end effector will move in Cartesian Space.



In executing a trajectory, a manipulator moves from its *initial position* to a desired *goal (final) position*. However, the motion may be:

Smooth (nice and secure)
 Rough (vibrations and damaging)

Trajectory in Cartesian Space

In general, the *task* of a robot manipulator is defined by a sequence of points which are denoted as end points and are stored in the robot's control computer.

Trajectory in Cartesian Space

Motions of a robot manipulator is described as the motions of the Tool Frame {T} relative to the Station Frame {S}.

Point-to-Point (PTP) Robotic Systems: The robot moves to a numerically defined location and then the motion is stopped. Then, the end-effector performs the required task with the robot being stationary. Upon completion of the task, the robot moves to the next point and the cycle is repeated. (Ex: Spot Welding Operations)

Therefore; in PTP robots, the path of the robot and its velocity while traveling from one point to the next is not important!

> Trajectory in PTP Cartesian Robotic System



X

2-End point

a_m

m

 $\theta_{\rm f} \stackrel{\bullet}{=} \theta$

 θ_{2}

 θ_1

 t_2

Example: Consider a simple case in which each joint of a PTP robot must move to its end point θ_f as fast as possible without exceeding a maximum ^{-a}_m admissible acceleration am and a maximum velocity V_m.

Desired Joint Trajectory consists of **3-segments:**

1. [0, t₁]; based on max. acceleration 2. $[t_1, t_2]$; based on *max. velocity* 3. $[t_2, t_f]$; based on max. deceleration

> Typical acceleration, velocity and position of an axial motion in PTP Robot.

8

Vm

 t_2

- Lets assume that the time durations of acceleration and deceleration segments are equal: $\{t_1 = t_f - t_2\}$. The control program must calculate the two switching times based on the initial and final joint values ($\theta_0 = 0$ and θ_f) and V_m and a_m .
- Joint Trajectory during:

1st Segment:
$$\theta(t) = \frac{a_m t^2}{2}, \quad \theta_1 = \frac{a_m t_1^2}{2}, \quad V_m = a_m t_1$$

2nd Segment:

 \geq

$$\theta(t) = \theta_1 + V_m(t - t_1), \quad \theta_2 = \theta_1 + V_m(t_2 - t_1),$$

3rd Segment:

$$\theta(t) = \theta_2 + V_m(t - t_2) - \frac{a_m(t - t_2)^2}{2}, \quad \theta_f = \theta_2 + V_m t_1 - \frac{a_m t_1^2}{2}, \qquad \theta_2$$

From above equations we can write:

$$\theta_f = V_m t_2 \Longrightarrow t_2 = \frac{\theta_f}{V_m} \quad and \quad t_1 = \frac{V_m}{a_m}, \quad t_f = \frac{V_m}{a_m} + \frac{\theta_f}{V_m} \quad \theta_1$$

Typical acceleration, velocity and position of an axial motion in PTP Robot.

Continues Path (CP) Robotic Systems: In this system the robot tool performs the task while the axes of motion are moving (both robot and the tool are moving simultaneously, and the speed of each joint can be controlled independently). (Ex: Arc Welding Operations)

Therefore; in CP robot operations, the position of the robot's tool at the end of each segment, together with the ratio of axes velocities, determine the generated trajectory. Ex: variations in the velocity of the arc welding result in a non-uniform weld seam thickness (i.e. an unnecessary metal built-up or even holes)

Motions of a robot manipulator is described as the motions of the Tool Frame {T} relative to the Station Frame {S}.

To move the manipulator's Tool from {Tool}_i to {Tool}_f, there exists an infinite number of *trajectories*.

{Tool}

Trajectory in Cartesian Space

i: initial position of the toolf: final position of the tool

To provide more details about the desired trajectory, we sometimes define some *via points* (intermediate points) throughout the path.

via points

{Tool}

Trajectory in Cartesian Space

i: initial position of the toolf: final position of the tool

Path Points: a set of Via points plus Initial and Final points.

In executing a trajectory, it is generally desirable to smoothly move the manipulator from its *initial position* to a desired *final position*.

For Smooth Motion: We need to have position and velocity to be continues functions of time.

Trajectory in Cartesian Space

A Smooth Function: A function which is continues and has a continues first derivative.



 $\mathbf{T}_{\mathbf{f}}$

 $\{\boldsymbol{\theta}_{\mathbf{f}}\}$

{B}

Joint Space Schemes: Methods of path generation in which path shapes are described in terms of functions of joint angles.

- Each *path point* (via points + initial and final points) is specified in terms of a desired position & orientation of the *Tool frame* {T}, relative to the *Base frame* {B}.
 {T}_i
- In Cartesian Space a set of via points may be used to take the Tool frame from initial state to a final state.
- Each via and path point is converted into a set of desired joint angles by applying *inverse kinematics*.
- A Smooth Function is defined for each of n-joints that pass through the via and path points.
- The *time* duration required for each motion segment is the same for each joint, so that all joints will reach the via point at the same time.

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{**θ**_i

Joint Space Schemes

 $\mathbf{T}_{\mathbf{f}}$

 $\{\theta_{f}\}$

{B}

Joint Space Schemes:

Each via and path point is converted into a set of desired joint angles by applying *inverse kinematics*.

{Tool} frame => { θ_{vector} }

**

{by Inverse Kinematics} = > a set of $\{\theta_i$'s and θ_f 's}

- **Generate a** *Smooth Function* through all points.
- In between via points, the shape of the path, although rather simple in joint space, is complex if described in Cartesian space.
- Joint Space schemes are easiest to compute, since there is usually no problem with *singularities* of the mechanism.

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 $[\theta_i]$

Joint Space Schemes

{T}

- **Cubic Polynomials:**
- By applying *inverse kinematics*.

 $\{Tool\}_i \implies \{\theta_i `s \}$ $\{Tool\}_f \implies \{\theta_f `s \}$

We need to define a *smooth function* for each joint whose value at "t_i" is " θ_i ", and at "t_f" is " θ_f "

There exist many smooth functions for $\theta(t) = ?...$



 $\{\theta_i\}$

 $\{\mathbf{T}\}_{\mathbf{f}}$

 $\{\boldsymbol{\theta}_{\mathbf{f}}\}$



 $\theta(t)$

 $t_i=0$

Many path shapes

t_f

θf

 $\theta_i = \theta_0$

Cubic Polynomials:

For Smooth joint motion, we need to impose at least 4-*constraints* on $\theta(t)$ as:

 $\theta(0) = \theta_i = \theta_0$ $\theta(t_f) = \theta_f$ $\dot{\theta}(0) = 0$ $\dot{\theta}(t_f) = 0$

•

Continues in Velocity: Start and Stop at Zero Velocities

We need to define a *smooth function* for each joint whose value at " t_i " is " θ_i ", and at " t_f " is " θ_f "



Cubic Polynomials:

A Cubic Polynomials satisfies the above constraints.

$$\theta(t) = a_0 + a_1 t + a_2 t^2 + a_3 t^3$$
 (4-Coefficients)

 $\theta(0) = \theta_0 = a_0$ $\theta(t_f) = \theta_f = a_0 + a_1 t_f + a_2 t_f^2 + a_3 t_f^3$ $\dot{\theta}(0) = 0 = a_1$ $\dot{\theta}(t_f) = 0 = a_1 + 2a_2 t_f + 3a_3 t_f^2$



5th Order Polynomials:

•

- If we add the *acceleration constraints* at the beginning and end of the path; then we have 6-Constraints.
- If acceleration is continues, then vibration is diminished ••• (i.e. if $a_i = a_f = 0$) at the start and the stopping points.
- Hence, a 5th Order Polynomial would be sufficient to ♣. define the joint motion.

 $\theta(t) = a_0 + a_1 t + a_2 t^2 + a_3 t^3 + a_4 t^4 + a_5 t^5$ (6-Coefficients)







θ

 $\dot{\theta}_0$

t_f

 $t_0 = 0$

For *intermediate (via) points* at which you don't want the robot to stop, θ_{f} velocity constraints at the end of cubic polynomial is no longer zero.

 $\theta(0) = \theta_0$ $\theta(t_f) = \theta_f$ $\dot{\theta}(0) = \dot{\theta}_0$ $\dot{\theta}(t_f) = \dot{\theta}_f$

4-Constraints

 $\theta(t) = a_0 + a_1 t + a_2 t^2 + a_3 t^3$



$$\theta(t) = a_0 + a_1 t + a_2 t^2 + a_3 t^3$$



> Several Ways to specify the desired velocities at the *via points*:

- ***** By the user in terms of Cartesian linear and angular velocities (mapped into joint velocities by Jacobian Inverse)
- The system automatically choose...
- The system automatically choose such that the acceleration is continues...



Robot Motion Trajectory Generation Linear Function with Parabolic Blends: Another choice of path shape is to move *Linearly* from *initial* joint position " θ_0 " to the *final* joint

 $\theta(t)$

t₀=

t_f

(Linear Function)

position "0_f".

Linear Function Results in:

 Velocity to be *discontinuous* at the beginning and end of motion,
 Acceleration to be *discontinuous*

• **Undesirable** (*Rough Motion*)

Linear Function with Parabolic Blends:

- To avoid rough motion, we can *add a Parabolic Blend* to the linear function at each end.
- Adding Parabolic blends
 with constant acceleration (θ_b)
 results in smooth change in
 velocity.
- Linear function and two parabolic functions are splined together so that the entire path is continuous in *Position* and *Velocity*.



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(Linear Function with Parabolic Blends)

Linear Function with Parabolic Blends:

Assume both blends have the same time duration, and note that velocity at the end of the blend must be equal to the velocity of the linear segment.

For the Linear segment: $\dot{\theta}(t_b) = \ddot{\theta}_b t_b = \frac{\theta_h - \theta_b}{t_h - t_h} = (slope - speed)^{-\theta_f}$ For the **Blend** region: $\ddot{\theta}_{b} = Cons \tan t$ Integrating using I.C.: $\begin{cases} \dot{\theta}_b(0) = 0\\ \theta_b(0) = \theta_0 \end{cases}$ $\dot{\theta}_b = \dot{\theta}_b t + C_1 0$ $\theta_b = \frac{1}{2}\ddot{\theta}_b t^2 + C_1 t + C_2 \theta_0$



 $\theta(t)$

(Linear Function with Parabolic Blends)

Linear Function with Parabolic Blends:

 $\theta_b = \frac{1}{2} \ddot{\theta}_b t_b^2 + \theta_0$ at t_b , and let: $t=2t_h$

Combining the above relations, we get:

$$\ddot{\theta}_b t_b = \frac{\theta_h - \theta_b}{t_h - t_h} = \frac{\frac{\theta_f + \theta_0}{2} - \frac{1}{2} \ddot{\theta}_b t_b^2 - \theta_0}{\frac{1}{2} - \frac{1}{2} \dot{\theta}_b t_b^2} = \frac{\theta_h - \theta_0}{1 - \frac{1}{2} - \frac{1}{2} \dot{\theta}_b t_b^2} = \frac{\theta_h - \theta_0}{1 - \frac{1}{2} - \frac{1}{2} - \frac{1}{2} \dot{\theta}_b t_b^2} = \frac{\theta_h - \theta_0}{1 - \frac{1}{2} - \frac{1}{2} - \frac{1}{2} - \frac{1}{2} \dot{\theta}_b t_b^2} = \frac{\theta_h - \theta_0}{1 - \frac{1}{2} - \frac{1$$

 $\implies \overline{\ddot{\theta}_b t_b^2 - \ddot{\theta}_b t_b} + (\theta_f - \theta_0) = 0$

Where:

- t: Desired duration of motion
- $\ddot{\theta}_{L}$: Acceleration acting during the blend region

Linear Function with Parabolic Blends:

Given any " θ_f ", " θ_0 ", and t, we can follow any of the paths given by choices of $\dot{\theta}_b$ and t_b which satisfy equation "*".

$$\ddot{\theta}_b t_b^2 - \ddot{\theta}_b t_b + (\theta_f - \theta_0) = 0$$

You may pick θ_b and solve for t_b ?

$$t_{b} = \frac{t}{2} - \frac{\sqrt{\ddot{\theta}_{b}^{2}t^{2} - 4\ddot{\theta}_{b}(\theta_{f} - \theta_{0})}}{2\ddot{\theta}_{b}} \ge 0$$

$$\ddot{\theta}_{b}^{2}t^{2} \ge 4\ddot{\theta}_{b}(\theta_{f} - \theta_{0}) \Rightarrow \ddot{\theta}_{b} \ge \frac{4(\theta_{f} - \theta_{0})}{t^{2}}$$

Linear Function with Parabolic Blends:

You may pick $\dot{\theta}_{and}$ solve for t_{b} ?

$$t_{b} = \frac{t}{2} - \frac{\sqrt{\ddot{\theta}_{b}^{2}t^{2} - 4\ddot{\theta}_{b}(\theta_{f} - \theta_{0})}}{2\ddot{\theta}_{b}}$$
$$\ddot{\theta}_{b}^{2}t^{2} \ge 4\ddot{\theta}_{b}(\theta_{f} - \theta_{0}) \Rightarrow \ddot{\theta}_{b} \ge \frac{4(\theta_{f} - \theta_{0})}{2}$$

= Equality means linear segment has zero length (Path is composed of two blends with equivalent slope).

> As the acceleration $\ddot{\theta}_b$ increases, the blend region becomes shorter and shorter. In the limit when $\ddot{\theta}_b \longrightarrow \infty$, we are back to the simple linear interpolation case.

Linear Function with Parabolic Blends:

Adding via points:

 $\theta(t)$

θ

θ

 $t_0 = 0$

(Linear Function with Parabolic Blends)

t_f

Chapter 7 Exercises:

7.3, 7.7, 7.8, 7.9, 7.11, 7.12

Chapter 8 Exercises:

8.1, 8.2, 8.3, 8.4, 8.8